











charge in	n cfs				Cadmium	Concentra	ition Coef	ficients
	Intercept c	oefficient					B Ir	ntercept
	Runoff		Low Flow Nove	ember-March	/	<del>۱</del> 72	0.000	1.51469
M34	-2.771	0.394	-2.28954	0.38718	N	/134	0.004	0.09818
CC48	1.752	0.130	6.77165			CC48	0	2.49092
A68	-11.131	0.498	-3.62869_	0.45153		\68	_	1.82408
7,00	-11.101	0.430	-3.02009_	0.45155	Ľ	100	0	1.02400
Discharge R	Relationships am	ong the thre	e gages					
	MONTH	J	F	M	Α	M	J	J
	Intercept	1	1	1	1	1	1	1
	A 72	64	63	77	155	682	1196	624
	M34	22	22	28	58	266	468	243
	CC48	14	13	15	22	91	158	83
	A68	25	25	31	66	329	585	300
	Ground wate	3	3	3	9	-3	-14	-2
1/(1+BQ) Di	scharge Repres	entation						
	A 72	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
	M34	0.9175	0.9188	0.9008	0.8110	0.4847	0.3481	0.5072
	CC48	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
	A68	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
Date variabl	es							
	sin	0.1552	0.6358	0.9276	0.9887	0.7862	0.3629	-0.1441
	cos	0.9879	0.7719	0.3737	-0.1496	-0.6180	-0.9318	-0.9896
	sin1	0.3066	0.9815	0.6932	-0.2959	-0.9717	-0.6763	0.2852
	cos1	0.9518	0.1916	-0.7207	-0.9552	-0.2361	0.7366	0.9585
	Consent	1	1	1	1	1	1	1
A72	Intercept	1	1	1	1	1	1	1
	BQ	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
	sin	0.1552	0.6358	0.9276	0.9887	0.7862	0.3629	-0.1441
	cos	0.9879	0.7719	0.3737	-0.1496	-0.6180	-0.9318	-0.9896
	sin1	0.3066	0.9815	0.6932	-0.2959	-0.9717	-0.6763	0.2852
	cos1	0.9518	0.1916	-0.7207	-0.9552	-0.2361	0.7366	0.9585
	Consent							
A72 Con	centration	0.9	1.3	2.0	2.4	2.2	1.6	1.1
M34	Intercept	1	1	1	1	1	1	1
	BQ .	0.9175	0.9188	0.9008	0.8110	0.4847	0.3481	0.5072
	sin	0.1552	0.6358	0.9276	0.9887	0.7862	0.3629	-0.1441
	cos	0.9879	0.7719	0.3737	-0.1496	-0.6180	-0.9318	-0.9896
	sin1	0.3066	0.9815	0.6932	-0.2959	-0.9717	-0.6763	0.2852
	cos1	0.9518	0.1916	-0.7207	-0.9552	-0.2361	0.7366	0.9585
	Consent	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000
M34 Concer	ntration	1	1	1	1	1	1	0

CC 48	Intercept	1	1	1	1	1	1	1	
	BQ	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	
	sin	0.1552	0.6358	0.9276	0.9887	0.7862	0.3629	-0.1441	
	cos	0.9879	0.7719	0.3737	-0.1496	-0.6180	-0.9318	-0.9896	
	sin1	0.3066	0.9815	0.6932	-0.2959	-0.9717	-0.6763	0.2852	
	cos1	0.9518	0.1916	-0.7207	-0.9552	-0.2361	0.7366	0.9585	
	Consent	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	
CC 48 Cor	ncentratrion	2	1	2	3	3	3	3	
A68	Intercept	1	1	1	1	1	1	1	
	BQ	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	
	sin	0.1552	0.6358	0.9276	0.9887	0.7862	0.3629	-0.1441	
	cos	0.9879	0.7719	0.3737	-0.1496	-0.6180	-0.9318	-0.9896	
	sin1	0.3066	0.9815	0.6932	-0.2959	-0.9717	-0.6763	0.2852	
	cos1	0.9518	0.1916	-0.7207	-0.9552	-0.2361	0.7366	0.9585	
	Consent	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	1.0000	
A68 Co	ncentration	2	2	3	3	2	2	1	
Concentra	itio	1	1	2	2	2	1	1	
Load in po	ounds per day								
	Sum	0	0	1	2	7	9	3	
	A72	0	0	1	2	8	10	4	
	% Difference	0.49	0.09	-0.06	-0.09	-0.12	-0.14	-0.14	
	RPD	0.40	0.08	-0.06	-0.10	-0.13	-0.15	-0.15	

dmium Conce	ntrat	ion C	oefficie	ents				
	BQ	sin		cos	sin1	C	cos1	Consent
		0	0.32001	-0.190	32 -0	0.15579 <b>_</b>	-0.48788	0.000
	1.061	68	0.13396	-0.045	85 -0	0.19308_	-0.24108	0
		0	-0.33663	-0.622	45 -0	0.47908_	-0.16659	0
		0	0.40996	0.285	84 -(	0.21475	-0.47368	0
		A	S		0	N	D	
	_	1	1		1	1	1	
		68	187		42	92	70	
		03	71		53	33	25	
		37	26		20	16	14	
	1	22	82		60	38	28	
		6	8	i	9	4	3	
	1.00	00	1.0000	1.000	00	1.0000	1.0000	
	0.70	87	0.7792	0.82	47	0.8824	0.9097	
	1.00	00	1.0000	1.000	00	1.0000	1.0000	
	1.00	00	1.0000	1.000	00	1.0000	1.0000	
	-0.62	71	-0.9360	-0.98	78	-0.7716	-0.3573	
	-0.77		-0.3521			0.6361		
	0.97		0.6591			-0.9816	-0.6674	
	0.21	35	-0.7521	-0.95	16	-0.1908	0.7447	
		1	1		1	1	1	
	4.00	1	1 0000		1	1	1 0000	
	1.00		1.0000			1.0000	1.0000	
	-0.62		-0.9360			-0.7716	-0.3573	
	-0.77		-0.3521			0.6361		
	0.97		0.6591			-0.9816	-0.6674	
	0.21	35	-0.7521	-0.95	10	-0.1908	0.7447	
	1	.2	1.5	1.	.7	1.4	1.0	
		1	1		1	1	1	
	0.70		0.7792			0.8824	0.9097	
	-0.62		-0.9360			-0.7716	-0.3573	
	-0.77		-0.3521			0.6361	0.9340	
	0.97		0.6591			-0.9816	-0.6674	
	0.21		-0.7521			-0.1908	0.7447	
	1.00		1.0000			1.0000	1.0000	
		1	1		1	1	1	
		•	•		•	•	•	

1	1	1	1	1	
1.0000	1.0000	1.0000	1.0000	1.0000	
-0.6271	-0.9360	-0.9878	-0.7716	-0.3573	
-0.7789	-0.3521	0.1556	0.6361	0.9340	
0.9769	0.6591	-0.3074	-0.9816	-0.6674	
0.2135	-0.7521	-0.9516	-0.1908	0.7447	
1.0000	1.0000	1.0000	1.0000	1.0000	
3	3	3	3	2	
1	1	1	1	1	
1.0000	1.0000	1.0000	1.0000	1.0000	
-0.6271	-0.9360	-0.9878	-0.7716	-0.3573	
-0.7789	-0.3521	0.1556	0.6361	0.9340	
0.9769	0.6591	-0.3074	-0.9816	-0.6674	
		-0.9516	-0.1908	0.7447	
U.Z.130	-U./ DZ I				
0.2135 1.0000	-0.7521 1.0000	1.0000	1.0000	1.0000	
1.0000	1.0000	1.0000	1.0000	1.0000	
1.0000	1.0000	1.0000	1.0000	1.0000	
1.0000 <b>1</b>	1.0000 <b>2</b>	1.0000 <b>2</b>	1.0000 <b>2</b>	1.0000 <b>2</b>	
1.0000 <b>1</b>	1.0000 <b>2</b>	1.0000 <b>2</b>	1.0000 <b>2</b>	1.0000 <b>2</b>	
1.0000 <b>1</b>	1.0000 <b>2</b>	1.0000 <b>2</b>	1.0000 <b>2</b>	1.0000 <b>2</b>	
1.0000 <b>1</b>	1.0000 <b>2</b> 1	1.0000 <b>2</b> 2	1.0000 <b>2</b> 2	1.0000 <b>2</b> 1	
1.0000 <b>1</b> 1	1.0000 <b>2</b> 1	1.0000 <b>2</b> 2	1.0000 <b>2</b> 2	1.0000 <b>2</b> 1	
1.0000 <b>1</b> 1	1.0000 <b>2</b> 1	1.0000 <b>2</b> 2	1.0000 <b>2</b> 2	1.0000 <b>2</b> 1	

A72								
	Chronic TV	S at A72			Pr	edicction I	Equation C	oefficients
	a2 b	2					AluminumC	
Cd	-3.49	0.7852		В		0.006	1.000	0.006
Cu	-1.7428	0.8545		In	tercept	82.304	-26.540	1.020
Mn	5.8743	0.3331		В	Q	200.676?	5610.562	1.466
Zn	0.8669	0.8473		si	n	16.936	158.116	0.599
				CC	os	48.860	40.749	0.066
				si	n1	15.385	127.998	-0.265
				CC	os1	-5.633	6.691	-0.292
I				C	onsent			
	Month	J	F	M	Α	M	J	J
	Q	64	63	77	155	682	1196	624
	Hardness	277	290	268	196	91	53	72
	Al ch	87	87	87	87	87	87	87
	Cd ch	2.2	2.3	2.1	1.7	1.0	0.6	8.0
	Cu ch	11	11	10	8	4	3	3
	Mn ch	2317	2352	2290	2064	1598	1333	1482
	Zn ch	279	290	271	208	109	68	90

M 34								
			Predic	ction equa	tion coeffi	cients		
		Hardness Alu	minum	Cadmium	Copper	Iron	Zinc	
	В	0.013	1.00	0.021	0.123	0.06521	0.021	
	Intercept	60.05228315	.10361	0.91724	14.65129	77.70523	205.25873	
	BQ	205.02801338	.29032	0.60966	00.98354	370.29706	378.11589	
	sin	9.24827)69	.03843	0.26911	14.16661	-89.38888	88.77920	
	cos	32.30173379	.08681	0.20991	10.17487	38.04002	85.94018	
	sin1	435	.43127	-0.12214	1.04278	186.24646	-17.99615	
	cos1	123	.10453	-0.14689	-3.82920	-12.30367	-45.60154	
	consent	-265	.10754	-	-10.75402	35.80515	-98.00378	
		_	_		_		_	_
	MONTH	J	F	M	Α	M	J	J
Avg monthly	Q	22	22	28	58	266	468	243
	Hardness	255	241	226	170	86	60	76
Chronic Stan	Al, ch	87	87	87	87	87	87	87
	Cd,ch	2.1	2.0	1.9	1.5	0.9	0.7	0.8
	Cu ch	20	19	18	14	8	6	7

M	ln 2253	3 2212	2163	1969	1571	1389	1504
Zn	ch 260	248	235	185	104	76	93

A68 Anima	as at Silve	erton						
		Pre	ediction	equation c	oefficients			
		Hardness Ca		•	Mangane:			
E	3	0.011na		na	0.010	0.016		
	ntercept	37.945	2.395	5.783	258.473	304.617		
E	3Q .	165.600			1371.923	644.136		
s	sin		1.712	2.049	611.024	315.451		
c	cos		0.140	0.729	81.662	-18.603		
s	sin1		-0.250	-1.520	16.031	-33.783		
c	cos1		-1.185	-0.472	-263.628	-140.108		
	Мау		-1.936	2.261	-258.699			
C	consent		-0.714	-1.828	411.428	-67.174		
Animas R	Month	J	F	М	Α	М	J	J
	Q	25	25	31	66	329	585	300
ŀ	Hardness	168	168	161	134	74	60	76
	Cd,tvs	1.5	1.5	1.5	1.3	8.0	0.7	8.0
	Cu tvs	14	14	13	11	7	6	7
	Mn tvs	1959	1961	1934	1818	1491	1393	1509
nic stand	Zn tvs	182	183	177	151	91	77	94

ction Equation Coeffic	cients			
•		Zinc		
0.100	0.048	0.014		
11.592	325.430	272.266		
-11.516	3156.248	697.432		
5.618	310.323	155.229		
5.955	262.025	37.490		
1.700	-72.066	-37.359		
-0.594	-177.065	-77.421		
-1.491				
	•			5
A	S	0	N	D
268	187	142	92	70
124	158	182	215	248
87	87	87	87	87
1.2	1.4	1.6	1.8	2.0
5	7	7	9	10
1772	1920	2013	2129	2233
141	173	195	225	255

		cute TVS			
	а	12 b	2 а	ı3 b	3
Cd		-3.828	1.128	-3.49	0.7852
Cu		-0.7703	0.9422	-1.7428	0.8545
Mn		4.4995	0.7893	5.8743	0.3331
Zn		0.8904	0.8473	0.8669	0.8473
	Α	S	0	N	D
	103	71	53	33	25
	126	151	192	217	253
	87	87	87	87	87
	1.2	1.4	1.7	1.8	2.0
	11	13	16	17	20

1783	1892	2050	2136	2246
144	167	205	227	258

а	2 b	2		
	-3.49	0.7852		
	-1.7428	0.8545		
	5.8743	0.3331		
	0.8669	0.8473		
Α	S	0	N	D
122	82	60	38	28
109	125	138	155	165
1.1	1.2	1.3	1.4	1.5
				14
				1947
				180
	a A	A S 122 82 109 125 1.1 1.2 10 11 1695 1777	-3.49 0.7852 -1.7428 0.8545 5.8743 0.3331 0.8669 0.8473 A S O 122 82 60 109 125 138 1.1 1.2 1.3 10 11 12 1695 1777 1836	A S O N 122 82 60 38 109 125 138 155 1.1 1.2 1.3 1.4 10 11 12 13 1695 1777 1836 1908